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Research Article

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Exploring use of quality by design (QbD) principles for development of modified release omeprazole pellets

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ABSTRACT

The present study was aimed to develop modified release pellet of Omeprazole (OMP) applying various tools of Quality by Design (QbD). Sugar spheres were drug layered, barrier coated, extended coated and enteric coated in a fluid bed coater to achieve drug release extension. Based on previous knowledge and initial experimental data, failure mode and effect analysis (FMEA) method were further applied in the risk analysis for the parameters of pellets formulation. Central composite design (CCD) was employed to optimize OMP pellets selecting independent variables (% TEC in ER coat, % Enteric coat, % Extended coat) and responses (% drug release at 2, 4 and 8 hrs. Statistical analysis exhibited that the most significant factor affecting Y_1 was X_2 . Factor X3 had significant negative effect on drug release at 4 hrs and 8 hrs which can be mathematically proved by regression equation of Y_2 and Y_3 . Results of physicochemical characterization of OMP pellets revealed compendia compliance. Results of short term stability study indicated stable characteristics of developed formulation.

Keywords: Omeprazole, Quality by Design, Risk assessment, Pellets

INTRODUCTION

In an endeavor to combat various pathological states, drugs have been administered through various possible routes. Oral intake, amongst these routes, has unambiguously been the most sought after by the patients and manufacturers alike [1]. Development of an effective oral drug delivery system (DDS), however, invariably involves rational blending of diverse functional and non-functional polymers and excipients. Optimizing the formulation composition and the manufacturing process of such a drug delivery product to furnish the desired quality traits is, therefore, a Herculean task [1].

Quality by design (QbD) has become the answer to assist both industry and FDA to move towards a more scientific, risk based, holistic and proactive approach to pharmaceutical development. It encompasses designing and developing formulations and manufacturing processes which ensures predefined product specifications [2]. It identifies characteristics that are critical to quality from the perspective of patients, translates them into the attributes that the drug product should possess, and establishes how the critical process parameters can be varied to consistently produce a drug product with the desired characteristics [3].

Omeprazole (OMP) is a lipophilic drug, which behaves as a weak base and it is moderately soluble in alcohol and slightly soluble in water (pKa1=4.2 and pKa2=9.0) [4]. It is known to be very sensitive towards acids and therefore requires an effective enteric coating for oral applications [5].

Multiple-unit sustained-release dosage forms, such as pellets, are believed to have many therapeutic advantages in comparison with the single-unit dosage forms. They can distribute in the gastrointestinal tract (GIT) homogeneously thus maximizing drug absorption and reducing peak plasma fluctuations, minimizing the risk of local GI tract irritation and dose dumping [6]. Thus, in the present study modified release pellets of OMP were developed employing various principles of QbD.

EXPERIMENTAL SECTION

Materials

Omeprazole was obtained from Cadila Pharmaceuticals Limited (Gujarat, India). Klucel LF was obtained from Ashlan (Wilmington, USA). Hypromellose phthalate (HP 55) was received from Shinetshu (Japan). Triethyl citrate was offered by cognis (Germany). Sodium lauryl sulphate (Stepanol, USA), Crosspovidone (BASF, India), Talc (Luzenac) and empty hard gelatin capsule size 1 (ACG) were used as received.

Determination of OMP

Concentrations of OMP in dissolution medium were quantified HPLC assisted by UV detector. A Novapak C18 (250 x 4.6mm, 5μ) column and a mobile phase comprising of phosphate buffer (pH 7.4) and acetonitrile in the ratio of 60:40, v/v were used. The flow rate was maintained at 1.2 ml/min.

Ingredient			
Non pareil seeds (20/25 #)	(mg) 150		
Drug layering			
Omeprazole	40		
Hydroxy propyl cellulose USP-NF (Klucel LF)	7.5		
Hypromellose 3 cps	5		
Disodium hydrogen phosphate dehydrate	1		
Sodium lauryl sulphate	2		
Crospovidone	4.5		
Water	Q.S.		
Drug loaded pellets	210		
Barrier coating	10%		
Drug loaded pellets	10%		
Hypromellose 3 cps	17.5		
PEG 400	1.75		
Talc	1.75		
Water	Q.S.		
Barrier coated pellets	231		
Extended release coating	10%		
Eudragit NE 30D	19.26		
TEC	1.92		
Talc	1.92		
Water	93		
Extended release coated pellet (mg)	254.1		
Enteric coating	15%		
Hypromellose phthalate (HP 55)	29.325		
Talc	5.86		
TEC	2.93		
Acetone	Q.S.		
Enteric coated pellets	292.215		
Talc	0.785		
Enteric coated lubricated pellets (mg) in empty hard gelatin capsule Size 1	293		

Table 1. Formulation of modified release OMP pellets

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Preparation of drug-loaded pellets

Sugar spheres were drug layered, barrier coated, extended coated and enteric coated in a fluid bed coater using ingredients shown in Table 1. Drug layering dispersion was prepared by dissolving a binder (Klucel LF, Hypromellose 3 cps) and a wetting agent (SLS) in water, followed by addition of crospovidone and drug. The drug dispersion was sieved through a 60# screen (250 μ m) to remove any aggregates. The extended release coat dispersion shown in Table 1 was prepared and passed through a 60# screen and applied to the drug loaded beads. The seal-coated beads were then enteric coated, using Hypromellose phthalate (HP 55) and triethyl citrate (TEC) as the plasticizer. The enteric coating composition was prepared and applied on seal coated beads. The dispersion was passed through a 60# screen prior to application. Due to the small size of the beads, the spray rate, air flow, and product temperature were carefully monitored to ensure individual particle coating and to minimize potential agglomeration or electrostatic charge. The process parameters were as follows: rotational speed of plate: Inlet temperature (°C): 40-60; Bed temperature (°C): 30-40; Exhaust temperature (°C): 30-40; Atomization air pressure (kg/cm²): 1-3; Total pressure (kg/cm²): 2-6; Peristaltic Pump rpm: 1-20.

Application of QbD principles:

Risk assessment

Fish-bone diagram was constructed to identify the potential risks and corresponding causes. Based on previous knowledge and initial experimental data, failure mode and effect analysis (FMEA) method were further applied in the risk analysis for the parameters of pellets formulation. Each variable (potential failure mode) was scored in terms of severity (S), detectability (D) and probability (P). More broadly, Severity is measure of the possible consequences of a failure mode affecting on the safety and efficacy of the final product. Detectability defined that a failure mode can be detected. The final parameter probability is considered as the occurrence probability or the likelihood of a failure. For each risk, S, D, P scores were multiplied together to produce a "Risk Priority Number" (RPN), RPN = S * D * P, which represents the overall magnitude of the risk. We ranked S, (1: No impact - have no influence on product quality, 2: Low impact - have little influence on product quality, 3: Moderate impact - have moderate influence on product quality, 4: High impact - have severe influence on product quality), D (1: Failure can be detected ever time., 3: Failure can be detected in some cases., 5: Failure cannot be detected) and P (1: Rare - failure is rare to happen., 3: Occasional - failure happens sometimes., 5: Frequent - failure is common to happen.). Maximum RPN of 100 and minimum RPN of 1 are possible. Any formulation variable or process parameter with an higher RPN was regarded as a potential critical factor, that is, potential risks are evaluated by subsequent process characterization studies since it possibly has a potential impact on CQAs and in consequence on product safety and efficacy, while factors with a lower RPN were eliminated from further study [7, 8].

Application of central composite design (CCD) [9]

After opting for the most important factors influencing the performance of the produced OMP pellets, a three-factor, three-level CCD was developed to explore the optimum levels of these variables. This methodology consisted of three groups of design points, including three-level factorial design points, axial or star points, and centre points. Therefore, three selected independent variables (% TEC in ER coat, % Enteric coat, % Extended coat) were studied at five different levels coded as $-\alpha$, -1, 0, +1, and $+\alpha$. The value for alpha (1.68) was intended to fulfill the rotatability in the design. Percentage drug release at 2 hrs, 4 hrs and 8 hrs were selected as dependent variables. According to the CCD matrix generated by Design-Expert software (Trial Version 7.1.6, Stat-Ease Inc., MN), a layout of 17 experiments was constructed.

Validation of CCD

The applied CCD was further validated by standard error graph. Standard error graph is a contour plot showing the standard error of prediction for areas in the design space. These values are reflective of the design only, not of the response data. For acceptable criterion this graphs to have relatively low standard error (approximately 1.0 or lower) across the region of interest [10].

Confirmation tests of model

To verify the accuracy and robustness of the model, two different combinations were chosen at different levels of the selected factors within and outside of design space (DS). Formulations at those compositions were analyzed and further compared the observed responses with the predicted [11].

Characterization of OMP pellets [12, 13]:

Physicochemical characterization

(a) Loading of pellets into capsules

The pellets which are optimized after the trials were checked for the bulk density and were loaded into hard gelatin capsules size 1 with automatic capsule filling machine (Rimek formulations).

(b) Weight variation test

Ten capsules were individually weighed and the contents were removed. The emptied capsules were individually weighed and the net weight of the contents was calculated by subtraction and the percent weight variation was calculated by using the following formula.

$$Weight variation = \frac{(Wt of Capsule - Average weight)}{*100}$$

Average wt of capsule

Weight variation should not be more than 7.5 %.

(c) Lock length

Ten individual capsules were taken from formulation trial batch and lock length was measured manually by using vernier calipers and average of ten capsules was noted.

(d) Friability and Sphericity:

A friability tester (CS-2, Tianjin, China) was used to tumble 10 g of pellets for 100 rpm. After friability testing, the pellets were sieved through a sieve. The weight of loss (F %) after testing was calculated as follows:

$$F(\%) = \frac{Wo - W}{Wo} * 100$$

Where, Wo is the initial weight of pellets before friability testing and W is the weight of pellets retained after friability testing. The testing was carried out in triplicate.

The one-plane-critical-stability (OPCS) was used to estimate the sphericity of the pellets [14]. The value of the OPCS was the angle between a horizontal plane and a tilted plane of maximum stability of the pellets staying on that plane. Each testing was carried out in triplicate.

In vitro drug release study

The OMP pellets were subjected to *in vitro* drug release for 12 hrs in a calibrated USP dissolution test apparatus (Electrolab, Model TDT 06-T, Mumbai, India) equipped with paddle employing 900 mL dissolution media. The dissolution media was changed after 2 h from 0.1N HCl (pH 1.2) to phosphate buffer (pH 6.8). The paddles were rotated at 50 rpm and the dissolution medium was maintained at a temperature of 37 ± 0.5 °C throughout the experiment. Five ml aliquots were withdrawn and analyzed by HPLC method as mentioned above. Five ml of fresh dissolution media was added after each withdrawal to maintain the volume of dissolution media. The study was carried out in triplicate.

Drug release kinetics

To investigate the kinetics of drug release from OMP pellets, the data of *in vitro* drug release were fitted to different models. In house developed FORTRAN language based program was used to fit zero order, first order, Higuchi, Hixson-Crowell, Korsmeyer-Peppas, and Weibull models. Appropriate drug release kinetic model was selected based on least SSR, least Fisher's ratio (F) and maximum R^2 [15].

Stability Studies

The optimized OMP pellets were charged for the accelerated stability studies as per ICH guidelines ($40 \pm 2^{\circ}$ C and 75 ± 5% RH) for a period of 3 months in stability chambers (Model-TH 90 S, Thermolab, India). They were placed in flint vials and hermetically sealed with rubber plugs and aluminum caps. The samples were taken out at 30, 60 and 90 days and evaluated for the various physicochemical parameters [16].

RESULTS AND DISCUSSION

QTPP of OMP pellets and CQA identification

QTPP for OMP pellets are listed in Table 2. According to scientific prior knowledge and preliminary studies, % drug release at 2 hrs, % drug release at 4 hrs and % drug release at 8 hrs were selected as CQA [17].

Attribute	QTPP				
Final Dosage form	Capsule				
Type of core content	Pellets				
Route of administration	Oral				
Appearance	Spherical shape				
Strength	40 mg				
In vitro release	% drug release at 2 hrs: 0-5%				
	% drug release at 4 hrs: 20-22%				
	% drug release at 8 hrs: 80-85%				
Friability	<1.0%				
Impurity	Below safety threshold				
Assay	Acceptable limit				
Content uniformity	Acceptable limit				

Table 2. QTPP for OMP pellets

Risk assessment

An Ishikawa diagram was plotted, in accordance with ICH Q8 R2 guideline, to identify an initial list of potential high risk factors that influenced the quality of the OMP pellets (Figure 1). It could be seen that four main causes (formulation, process, environmental and personnel factors) were identified.



Figure.1: Ishikawa diagram depicting factors that may have impact on the critical quality attribute (CQA) of the OMP pellets

Figure 2 presents the results of risk analysis, which were achieved based on prior knowledge and preliminary study. It could be seen that three potential high risk variables (RPN>35) were identified. Then preliminary experiment was carried out to select the auxiliary excipients and non significant process parameters (data not shown). Further to understand the main, interactive and polynomial effect of these causative factors on selected CQAs, CCD was employed.



Figure.2: RPN score after FMEA risk assessment

Validation of CCD

Figure 3 shows the standard error graph of applied CCD which indicates the standard error maximally 0.56 reflecting efficacious prediction power of proposed factorial design.



Figure.3: Standard error graph of applied CCD

Application of CCD

The experimental run with factors and corresponding responses were presented in Table 3.

Run	X ₁	X_2	X ₃	Y ₁		Y ₂		Y ₃	
1	-1	-1	-1	14.65	±2.09	30.64±3.14		94.32±6.24	
2	1	-1	-1	13.56	±1.68	33.56	±4.05	99.56±3.61	
3	-1	1	-1	5.84±	±0.62	30.74±2.37		94.65±2.84	
4	1	1	-1	7.65±	±0.85	5 32.65±2.14		99.68±3.41	
5	-1	-1	1	11.45	±1.07	±1.07 20.11±1.98		75.23±2.04	
6	1	-1	1	11.85	±1.34	21.11±1.84		79.65±2.31	
7	-1	1	1	5.21±	0.012	18.86	±0.96	76.58±3.14	
8	1	1	1	6.74±	0.034	20.98	±1.24	79.82±1.65	
9	-1.68	0	0	6.75	±0.44	21.09±1.36		83.48±2.08	
10	1.68	0	0	8.34	±1.03	25.04±1.47		92.13±3.25	
11	0	-1.68	0	19.17	±2.61	23.91±2.57		88.91±2.46	
12	0	1.68	0	5.65±	±0.21	23.55±2.31		89.55±3.64	
13	0	0	-1.68	9.83±	9.83±0.55		±0.55 40.86±3.67		101.5±4.91
14	0	0	1.68	7.34±	±0.32	32 20.95±2.14		69.98±3.24	
15	0	0	0	8.4±0.26		26 24.64±3.24		89.64±4.31	
16	0	0	0	8.36±0.28		24.6	±1.6	89.6±2.59	
17	0	0	0	8.42±0.33		24.66	±3.12	89.66±3.09	
	Level and actual value								
Indepen	Independent variables -1		()		+1		
	X1	5		10		0		15	
	X2		10		15			20	
	X3		7		10 1		13		

Table 3. Experimental runs obtained from CCD and responses

 Y_1 varied from 5.21±0.012 to 19.17±2.61. Y_2 varied from 18.86±0.96 to 40.86±3.67. Y_3 varied from 75.23±2.04 to 101.5±4.91. The model explaining the effects of various factors on Y_1 was as follows:

Similarly, Y_2 and Y_3 can be equated in the form of following equations.

 $Y_{2} = 24.63 + 1.07X_{1} - 0.20 X_{2} - 5.86X_{3} + 0.014X_{1}X_{2} - 0.21 X_{1} X_{3} - 0.071X_{2}X_{3} - 0.53X_{1}^{2} - .30X_{2}^{2} + 2.24X_{3}^{2} + 0.27X_{1}X_{2}X_{3} - 0.071X_{2}X_{3} - 0.07X_{2}X_{3} - 0.07X_{3} - 0.$

 $Y_{3} = 89.64 + 2.38X_{1} + 0.22X_{2} - 9.51X_{3} - 0.17X_{1}X_{2} - 0.33X_{1}X_{3} + 0.13X_{2}X_{3} - 0.65X_{1}^{-2} - 0.15X_{2}^{-2} - 1.38X_{3}^{-2} - 0.12X_{1}X_{2}X_{3} - 0.12X_{1}X_{2}X_{3}$

Statistical analysis exhibited that the most significant factor affecting Y_1 was X_2 . Though, the factors X_1 and X_3 also had positive effect on Y_1 . The effect of X_2 on Y_1 was on negative, which further indicates that as the level of enteric coating is increased, initial release for 2 hrs is decreased.

Factor X_3 had significant negative effect on drug release at 4 hrs which can be mathematically proved by regression equation of Y_2 . As layer on extended coating is increased on pellets, drug diffusion from inner core is retarded. Similarly it had effect on drug release at 8 hrs with greater magnitude, which also proved extension of drug release at later stages by applying more coating layer.

Though the terms bearing probability value (p) more than 0.05 (95% Confidence interval) (non-significant) were omitted from the full linear regression models and further reduced model were evolved to get accurate and significant information about the responses [18]. The regression coefficients and p value for selected responses are summarized in Table 4.

Parameter	% Drug release	at 2 hrs (Y ₁)	% Drug release	at 4 hrs (Y ₂)	% Drug release at 8 hrs (Y ₃)		
rarameter	Co efficient	р	Co efficient	р	Co efficient	р	
X_1	0.45	0.0454	1.07	< 0.0001	2.38	< 0.0001	
X_2	-3.73	< 0.0001	-0.20	0.0120	0.22	0.0376	
X3	-0.84	0.0034	-5.86	< 0.0001	-9.51	< 0.0001	
X_1X_2	0.613	0.0405	0.014	0.8611	-0.17	0.1640	
X_1X_3	0.261	0.3102	-0.21	0.0296	-0.33	0.0247	
X_2X_3	0.311	0.2348	-0.071	0.3804	0.13	0.2681	
X_{1}^{2}	-0.286	0.1996	-0.53	0.0002	-0.65	0.0004	
X_2^2	1.299	0.0006	-0.30	0.0034	-0.15	0.1563	
X_{3}^{2}	0.0815	0.6958	2.24	< 0.0001	-1.38	< 0.0001	
$X_1X_2X_3$	-0.111	0.6536	0.27	0.0123	-0.12	0.3110	

Table 4. Regression coefficients and p value for % drug release at 2, 4 and 8 hrs

 $Y_1 = 8.39 + 0.45X_1 - 3.73 X_2 - 0.84X_3 + 0.613 X_1X_2 + 1.299 X_2^2$

 $Y_{2} = 24.63 + 1.07X_{1} - 0.20 X_{2} - 5.86X_{3} - 0.21 X_{1} X_{3} - 0.53X_{1}^{-2} - 0.30X_{2}^{-2} + 2.24X_{3}^{-2} + 0.27X_{1}X_{2}X_{3}$

 $Y_3 = 89.64 + 2.38X_1 + 0.22X_2 - 9.51X_3 - 0.33X_1X_3 - 0.65X_1^2 - 1.38X_3^2$

So, from the reduced models of Y_1 , Y_2 and Y_3 , it can be anticipated that selections of independent variables (X_1 , X_2 and X_3) are judicious, as main effect terms are present in all models. The interactive term (X_1X_2) had a significant effect on initial drug release while that of X_1X_3 had on drug release at intermediate and later stages. Polynomial terms also had remarkable effect on drug release. Response surface plots relating the effect of factors X_1 and X_2 on selected CQAs (Y1, Y_2 and Y_3) are presented in figure.4.



Figure.4: Response surface plots showing effect of % TEC in ER (X1) and % Enteric coat on % drug release at 2 hrs (Y1), % drug release at 4 hrs (Y2) and % drug release at 8 hrs (Y3)

Confirmation tests of model

To confirm applicability of evolved reduced model equations, check-point batches F18 (outside of design space) and F19 (with in design space) were formulated. The theoretical and experimental responses of $Y_1(\%)$, $Y_2(\%)$ and $Y_3(\%)$

for batch F18 were 9.36, 21.57, 81.23 and 9.55 ± 1.53 , 20.57 ± 12.19 , 79.86 ± 3.64 h, respectively, whereas that of batch F19 were 4.59, 19.53, 78.80 and 4.73 ± 0.52 , 20.11 ± 1.38 , 81.32 ± 2.06 respectively. The results confirmed predictive potential of the evolved models. Based on the results of *in vitro* drug release, batch F19 was considered as an optimized batch satisfying predetermined criteria in terms of % drug release at 2, 4 and 8 hrs. Figure 5 depicts overlaid contour plot which shows dark region of interest. F19 batch belongs to this design space.



Physiochemical characterization

The values of bulk density and tapped density of OMP pellets were 0.632 and 0.665 g/ml respectively. The lock length value of capsule was 18.64 mm. The weight variation in final optimized formulation was $1.05\pm0.022\%$. The sphericity value of developed OMP pellets were nearer to the 1.



Figure.6: In vitro dissolution profile of optimized batch (F19)

Drug release kinetics

In vitro drug release profile of batch F19 is presented in figure. 6. *In vitro* dissolution data of the optimized formulation F18 was fitted to various mathematical models (zero order, first order, Higuchi, Hixson-Crowell, Korsmeyer-Peppas, and Weibull) in order to describe the kinetics of drug release. An optimized formulation (F19) did not followed any model out of tried models perfectly as there were remarkable difference in SSR, F and R^2 values. The least SSR (713.56) and F (71.35) values obtained from zero order model which were significantly high to conclude the drug release kinetics (Table 5).

Parameter	Zero order	First Order	Higuchi model	Hixon – Crowell	Korsmeyer -Peppas	Weibull
\mathbb{R}^2	0.9548	0.94	0.86	0.95	0.96	0.94
F*	71.35	357.98	219.96	153.98	128.41	85.58
SSR**	713.56	3579.85	2199.61	1539.85	1155.73	770.22
Slope	0.1496	-0.003	4.05	0.004	1.32	1.57
Intercept	-5.59	4.86	-22.74	-0.24	-3.79	-4.20
n					1.31	

(*F is Fisher's ratio, **SSR is sum of square of residuals)

Stability study

An optimized formulation (F19) showed stable characteristics after stipulated time of stability testing. The results of the stability study are depicted in Table 6.

Table 6. Evaluation parameters for optimized batch subjected to stability study

Parameters	F19						
Farameters	Initial	1 month	2 months	3 months			
Drug content (%)	99.33±0.041	98.71±0.036	100.43±0.018	99.22±0.047			
Friability	0.76±0.0015	0.81±0.0034	0.85±0.0043	0.89±0.0019			
Physical degradation	No	No	No	No			
% Drug release after 8 hrs	81.32±2.06	83.64±3.11	79.34±1.98	80.42±3.11			

CONCLUSION

The present study revealed that the usefulness of the application of QbD principles to gain a fundamental understanding of formulation and processing factors affecting the OMP pellets. According EMEA analysis, % TEC in ER coat, % Enteric coat, % Extended coat were identified as high risk factors. These three factors were further used for CCD to develop DS. Reduced model equations stated the significance of main, interactive and polynomial effect on selected CQAs. So, in a nutshell, this study demonstrated that OMP pellets were successfully designed using QbD principles, and it can be used as successful dosage regimen in treatment of GIT diseases.

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