



## Experimental study of urea on SNCR removal of NO<sub>x</sub>

Quan Wang, Qingcheng Wang\* and Jianjun Cai

Shanghai Institute of Technology, Shanghai, China

---

### ABSTRACT

Nitrogen oxide is one of the main pollutants in the atmosphere, so it is very important to study the technology of nitrogen oxide emissions. In this paper, urea being used as reducing agent, the denitration effect and law of various experimental conditions on SNCR technology were studied, by changing the reaction temperature, NSR, O<sub>2</sub> concentration and the other conditions. Experimental results showed that the reaction temperature, NSR and O<sub>2</sub> concentration had a great influence of urea on SNCR removal of NO<sub>x</sub>; the optimum denitration temperature of SNCR was about 925 °C, at the same time the maximum efficiency was 81%; the optimal temperature window of reduction was 875-1025 °C, within this interval efficiency over 50%; the optimal NSR was 1.5; denitration efficiency achieved the maximum value (83%) at 1100 °C in anaerobic conditions; in aerobic conditions, the maximum efficiency was achieved at about 925 °C; the optimum O<sub>2</sub> concentration was between 1% and 4%.

**Keywords:** Nitrogen oxide, urea, SNCR, denitration efficiency.

---

### INTRODUCTION

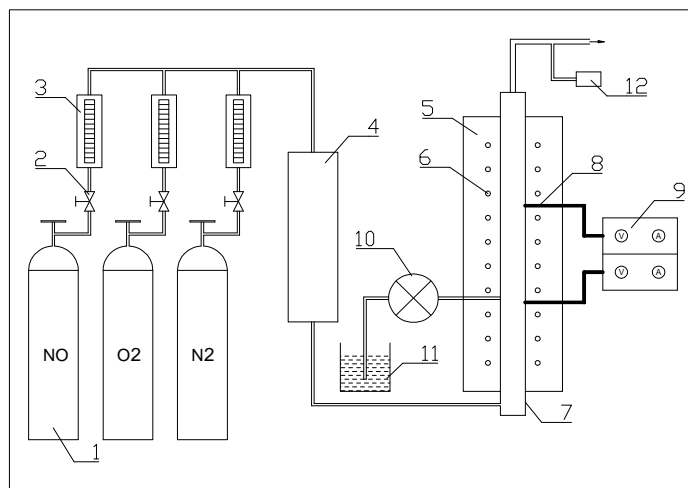
Nitrogen oxide (NO<sub>x</sub>) is a compound composed of nitrogen, oxygen, with the common nitrogen oxides NO, NO<sub>2</sub>, N<sub>2</sub>O, N<sub>2</sub>O<sub>5</sub>, etc. NO<sub>x</sub> in the air is often NO and NO<sub>2</sub>, of which NO accounts for 90% or above. NO<sub>x</sub>, one of the main pollutants in the atmosphere, could lead to acid rain, photochemical smog, haze and a series of urban environmental problems, and has a huge hazard on human health and ecological environment<sup>[1,2]</sup>. Therefore, it is very important to study the NO<sub>x</sub> removal technology.

Selective non-catalytic reduction (SNCR) technology is a NO<sub>x</sub> removal technology, which injects reducing agent with amino-group (ammonia, urea, ammonium bicarbonate) into a suitable temperature range (850-1050 °C), and reverts NO<sub>x</sub> in flue gas to N<sub>2</sub> and H<sub>2</sub>O without catalyst<sup>[3,4]</sup>. Because urea is a stable and nontoxic solid, easy to store and transport, NO<sub>x</sub>OUT process<sup>[5]</sup> for using urea (NH<sub>2</sub>CONH<sub>2</sub>) as nitrogen reducing agent is widely applied and studied. Research by scholars of SNCR technology showed that denitration effect on SNCR was related to many factors, such as reaction temperature, ammonia and nitrogen ratio(NSR), oxygen concentration and additive<sup>[6]</sup>. In this paper, urea being as a reducing agent, by changing the experimental conditions (reaction temperature, NSR, O<sub>2</sub> concentration), this article took a research on the impact and rule of various experimental conditions on SNCR denitration effect in NO<sub>x</sub>OUT process, and found experimental conditions and parameters, which made the SNCR denitration effects optimum.

### EXPERIMENTAL SECTION

#### Experimental equipment

Experiments were carried out on a self-made vertical experimental station. The experimental system was composed of gas distribution section, electric furnace reactor, reducing agent injection device, flue gas analyzer and other components. The experimental apparatus was shown in Fig. 1.



1- Gas collecting bottle; 2- Flow control valve; 3- Glass rotor flowmeter; 4- Mixer; 5- Electric heating furnace; 6- Silicon carbide; 7- Corundum tube; 8- Thermo-couple; 9- Temperature controller; 10- Peristaltic pump; 11- Urea solution; 12- Flue gas analyzer  
Fig. 1 Experimental system schematic

The reactor, vertically arranged corundum tube ( $\varnothing 60\text{mm} \times 700\text{mm}$ ), was arranged in an electric heating furnace. Electric heating furnace with silicon carbide as a heating element, through temperature controller and thermocouple formed temperature feedback system, which could effectively control and measure the furnace temperature, with the control accuracy of  $\pm 5^\circ\text{C}$  and the highest temperature of  $1350^\circ\text{C}$ . Three kinds of gases, NO, O<sub>2</sub>, N<sub>2</sub>, through flow control valve and glass rotor flowmeter, got into mixer with certain proportion and formed a simulated flue gas, which replaced NO<sub>x</sub>. Simulated flue gas entered corundum tube reactor, then reacted with urea for injection into furnace under certain conditions. The urea solution injection into position from the corundum tube bottom was 210mm. Flue gas was measured by the KM9106 portable flue gas analyzer of British KANE company and America IST series IQ-1000 multifunction gas detector.

### Experimental method

Experiments used urea as reducing agent, with mass fraction of urea solution 2% and reaction temperature range from  $750^\circ\text{C}$  to  $1150^\circ\text{C}$ . Following the initial experimental conditions, the total flow of simulated flue gas was constant 2L/min (standard condition), the initial NO concentration was  $300 \mu\text{L/L}$ , NSR was 1.5, the O<sub>2</sub> concentration was 2%, and N<sub>2</sub> was balance gas. In this paper, the effects of temperature, NSR and O<sub>2</sub> concentration on denitration efficiency and ammonia leakage of SNCR were studied.

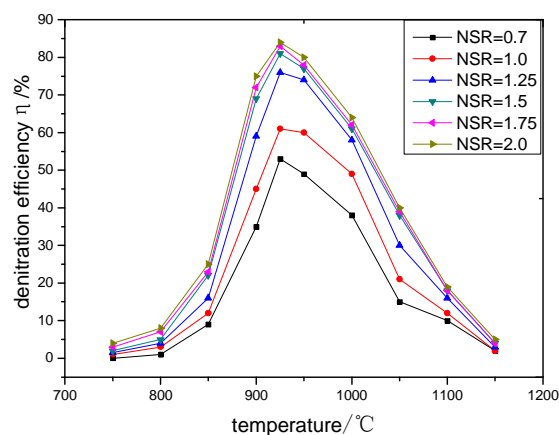
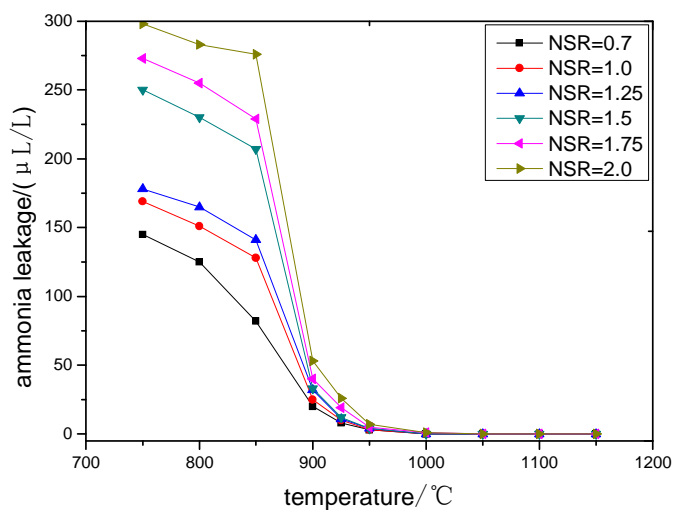
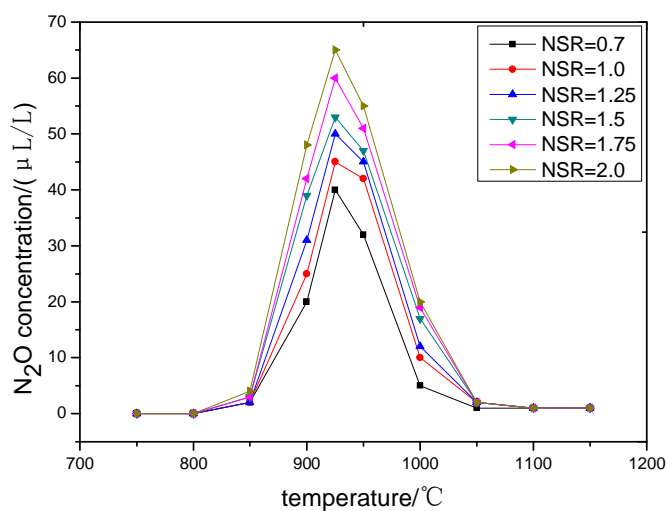
## RESULTS AND DISCUSSION

$$\text{denitration efficiency } \eta = \frac{\varphi_{(\text{NO}, \text{in})} - \varphi_{(\text{NO}, \text{out})}}{\varphi_{(\text{NO}, \text{in})}} \times 100\%$$

### Effect of temperature on SNCR

Because the temperature had a great influence on NO<sub>x</sub> reduction, the effects of temperature on denitration efficiency, ammonia leakage and N<sub>2</sub>O concentration were focused on.

As was shown in figures 2,3 and 4, the effects of temperature on denitration efficiency, ammonia leakage and N<sub>2</sub>O concentration in NO<sub>x</sub> removal of urea were obvious. From Fig.2, under different NSR conditions, DeNO<sub>x</sub> efficiency had an optimal temperature, about  $925^\circ\text{C}$ . When temperature was below  $800^\circ\text{C}$ , the concentration of OH, H, O active radicals was low to inhibit reduction of NO, so that denitration reaction was difficult to carry out and efficiency was less than 10%. When temperature was gradually increased, reaction rate of denitration increased, which caused reaction of urea reduction NO dominant and removal efficiency increasing rapidly. When temperature was  $925^\circ\text{C}$ , NO reduction efficiency reached a maximum value of 81% (NSR=1.5), that was to say that optimum denitration temperature was  $925^\circ\text{C}$ . When temperature continued to increase, NH<sub>3</sub> oxidation reaction rate was higher than NO reduction reaction rate, resulting in efficiency decrease with the increase of temperature. When temperature exceeded  $1150^\circ\text{C}$ , efficiency was lower than 10%. Only in  $875\text{--}1025^\circ\text{C}$ , efficiency was more than 50%, and it was the optimal temperature window.

**Fig.2** effect of temperature on denitration efficiency**Fig.3** effect of temperature on ammonia leakage**Fig.4** effect of temperature on N<sub>2</sub>O concentration

We could see from Fig. 3, the effect of temperature on ammonia leakage was obvious. Ammonia leakage was large at low temperature, because large ammonia decomposition by urea couldn't react on oxidation or reduction reaction to be consumed at low temperature. When the temperature was higher than 800°C, with the increase of temperature, the reduction of NO and the oxidation of NH<sub>3</sub> were accelerated, and the two reactions were consumption of NH<sub>3</sub>, so ammonia leakage concentration in flue gas decreased rapidly. At 950°C, ammonia leakage concentration was below 10 μL/L. When temperature continued to rise, ammonia leakage was almost zero. Fig. 4 showed that N<sub>2</sub>O concentration was low, less than 5 μL/L, when temperature was below 850°C. With increasing temperature, the reaction of NH<sub>3</sub>+NO→N<sub>2</sub>O+H<sub>2</sub>O increased, so N<sub>2</sub>O concentration increased rapidly. When temperature was 925°C, N<sub>2</sub>O concentration reached a maximum value of 53 μL/L(NSR=1.5). When temperature continued to increase, that N<sub>2</sub>O began to decompose made N<sub>2</sub>O concentration decrease rapidly. when temperature reached 1050°C, N<sub>2</sub>O concentration was less than 5 μL/L.

According to Fig. 2 and Fig. 3, when temperature was higher than 925°C, ammonia concentration was low, and denitration efficiency decreased continually, which indicated that NH<sub>3</sub> was consumed largely and produced NO, also proved that oxidation of NH<sub>3</sub> played a main role. According to Fig. 2 and Fig. 4, denitration efficiency and N<sub>2</sub>O concentration reached the maximum value at 925°C.

### Effect of NSR on SNCR

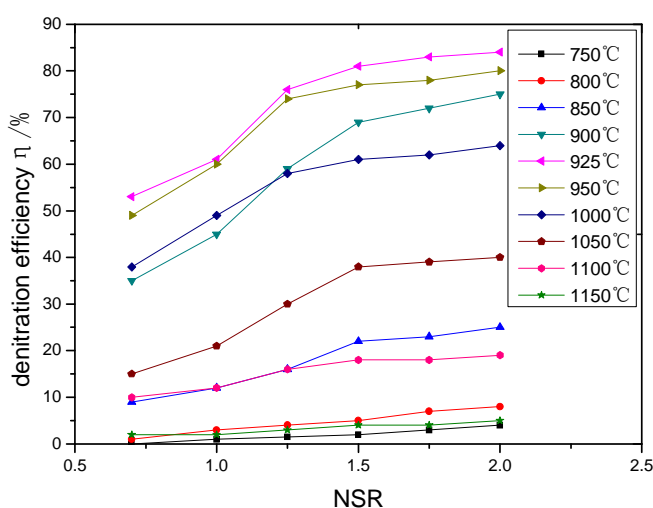


Fig.5 effect of NSR on denitration efficiency

Ammonia and nitrogen ratio (NSR) referred to the ratio of the actual and theoretical ammonia and nitrogen ratio. According to the chemical reaction equation, when NSR=1, it could completely remove NO. But for the influence of the actual process affected by factors such as the degree of mixing, NSR=1 couldn't achieve better denitration results, appropriate to increase the NSR value.

From Fig.5, the higher the NSR was, the higher denitration efficiency was. When NSR=1.5, the maximum DeNO<sub>x</sub> efficiency was 81%. But NSR was greater than 1.5, with the increase of NSR, increasing trend of removal efficiency was not obvious. when NSR=2, the maximum reduction efficiency was 84%. According to Fig. 3 and Fig. 4, the higher the NSR was, the higher ammonia leakage and N<sub>2</sub>O concentration were, not conducive to NO reduction.

Due to increasing NSR and the decomposition of urea to generate NH<sub>3</sub>, the excess NH<sub>3</sub> would lead to the increase of ammonia leakage concentration. At the same time, increasing NH<sub>3</sub> concentration would also accelerate the reaction, eventually to some extent resulting to N<sub>2</sub>O concentration increasing, so NSR should not be too large. Considering denitration efficiency, ammonia leakage and N<sub>2</sub>O concentration, the optimal NSR was 1.5.

### Effect of O<sub>2</sub> concentration on SNCR

O<sub>2</sub> was an important condition for SNCR reaction, both involved in NO reduction reaction, but also the NH<sub>3</sub> oxidation to NO. Therefore, it was essential to study the influence of O<sub>2</sub> concentration on the SNCR reaction.

As was shown in Fig.6, in the hypoxic conditions (O<sub>2</sub>=0%), denitration efficiency was very low when temperature was below 1000°C. With temperature gradually increasing, efficiency increased rapidly, reaching a maximum value at

1100 $\square$ . If temperature continued to increase, efficiency gradually decreased. In aerobic conditions, with the increase of temperature, efficiency at low temperature increased and it reached the maximum at 925 $\square$ . DeNO<sub>x</sub> efficiency decreased if temperature continued to rise. When temperature reached 1100  $\square$ , efficiency was very low. In aerobic conditions, trends of denitration efficiency on different O<sub>2</sub> concentration were basically the same, reaching the maximum at about 925  $\square$ , but removal efficiency was slightly different under different circumstances.

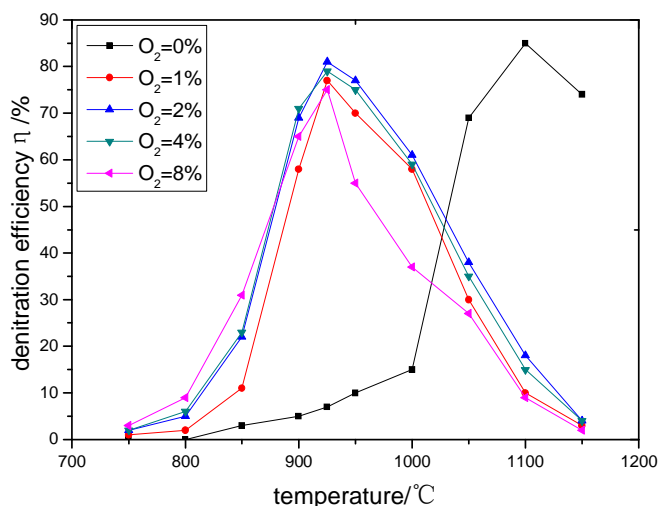


Fig.6 effect of O<sub>2</sub> concentration on denitration efficiency

On the Analysis of the reaction mechanism, OH, O and other active radicals were only formed by the reaction between H and H<sub>2</sub>O in the absence of oxygen. However the reaction was extremely slow and greatly inhibits the reduction reaction at low temperature. Therefore, denitration efficiency was extremely low at low temperature. As temperature increased, the concentration of OH, O active radicals increased. It made that reduction reaction could be carried out smoothly and denitration efficiency increased. In aerobic conditions, the concentration of OH, O active radicals increased rapidly with temperature increasing, so that efficiency also increased rapidly. But temperature exceeded a certain limit, the oxidation reaction of ammonia became dominant reaction, nitrogen oxides concentration in the flue gas was even more than the original concentration. From Fig.6, the maximum denitration efficiency in anaerobic conditions was higher than the one in aerobic conditions. A possible reason was that temperature of generating OH, O and active radicals were improved by anaerobic conditions. At the same time, the oxidation of ammonia was greatly suppressed, so that the reduction reaction was more dominant at optimum temperature and there would be a higher DeNO<sub>x</sub> efficiency compared to aerobic conditions.

From Fig.6, when O<sub>2</sub> concentration arrived at 1% , 2% , 4%, denitration efficiency was high and had little difference. Considering optimum temperature window (875-1025 $\square$ ), the optimum O<sub>2</sub> concentration was between 1% and 4%.

### Summary

The reaction temperature had a great influence of urea on SNCR removal of NO<sub>x</sub>. The optimum denitration temperature of SNCR was about 925 $\square$ , at the same time the maximum efficiency was 81%. The optimal temperature window of reduction was 875-1025 $\square$ , within this interval denitration efficiency over 50%. Ammonia leakage decreased rapidly with increasing temperature. When temperature was higher than 950 $\square$ , ammonia leakage concentration was below 10 $\mu$ L/L. With the increase of temperature, N<sub>2</sub>O concentration also increased at first and then decreased, and at 925  $\square$ , N<sub>2</sub>O concentration reached the maximum value of 53  $\mu$ L/L. The higher the NSR was, the higher denitration efficiency, ammonia leakage and N<sub>2</sub>O concentration were. And the optimal NSR was 1.5.

In anaerobic conditions, denitration efficiency achieved the maximum value of 83% at 1100 $\square$ . In aerobic conditions, the maximum efficiency was achieved at about 925 $\square$ . The optimum O<sub>2</sub> concentration was between 1% and 4%.

### REFERENCES

[1] H.D. Xu; Q.L. Zhang; C.T. Qiu; et al. Tungsten modified MnO<sub>x</sub>-CeO<sub>2</sub>/ZrO<sub>2</sub> monolith catalysts for selective catalytic reduction of NO<sub>x</sub> with ammonia. *Chemical Engineering Science*, 2012(76), 120–128.

- [2] S. Lee; K. Park; J.W. Park; et al. Characteristics of reducing NO using urea and alkaline additives. *Combustion and Flame*, **2005**(141), 200–203.
- [3] X. Hou; H. Zhang; M. Pilawska; et al. The formation of N<sub>2</sub>O during the reduction of NO by NH<sub>3</sub>. *Fuel*, **2008**(87),3271-3277.
- [4] M. Yu; W.J. YANG; Z.C. Chen; et al. Influence of H<sub>2</sub>O<sub>2</sub> additive on SNCR process. *Energy Engineering*, **2013**(3),45-49. (in Chinese)
- [5] T.D.B. Nguyen; T.H. Kang; Y.I. Lim; et al. Application of urea-based SNCR to a municipal incinerator: On-site test and CFD simulation. *Chemical Engineering Journal*, **2009**(152), 36-43.
- [6] Q.X. Cao; S.H. Wu; H. Liu; et al. Experimental Study of Selective Non-catalytic Reduction of NO by NH<sub>3</sub>. *Journal of engineering for thermal energy and power*, **2010**,25(1),87-90. (in Chinese)