

Research Article

# The approach of error calibration for three-axis magnetic heading sensor 

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#### Abstract

The accuracy of magnetic heading sensor is reduced by the impact of manufacturing technology and local magnetic interferences. The singularity of constraint matrix in traditional calibration algorithm leads to unstable results. Therefore, an improved least-square ellipsoid fitting method is proposed in this paper. The error source and the deviation mathematical model are introduced. On the basis of the analysis on singularity of the constraints matrix, parameter extraction by the improved least-square ellipsoid fitting method is given. The new method successfully overcomes the instability of the traditional algorithm, and reduces the computation load. Simulation and experimental results show that this method is effective in calibrating magnetic heading sensor. The heading precision of the sensor acquired after calibration is better than $0.42^{\circ}$.


Keywords: Magnetic heading sensor; error calibration; ellipsoid fitting; singularity

## INTRODUCTION

Magnetic heading sensors through to the earth's magnetic field measurement, indicates the course, unmanned aerial vehicle is one of the important sensor on the unmanned aerial vehicle. But because of the influence of the magnetic material on board and the limitation of the sensor preparation, encapsulation process, direct measurement of sensor data contains a variety of error, error compensation should be carried out before use. At present main compensation methods of ellipse fitting, kalman filter and neural network, ellipsoid fitting, etc. The least-squares ellipse fitting method [1] is simple, but to the compensation effect of three axis sensor is limited; Kalman filter [2] [3], the neural network needs higher precision reference datum; Ellipsoid fitting method based on iterative method [4-5] are susceptible to the initial estimate and the noise influence and spread, and large amount of calculation; Traditional least squares fitting ellipsoid method to achieve high precision compensation [6], but the algorithm exist due to the instability problems caused by the constraint matrix is singular.

In order to solve this problem, this paper puts forward the improved least-squares ellipsoid fitting method. The method is based on the assumption ellipsoid, error compensation coefficient was calculated by the least square method, the constraint has been solved by the matrix decomposition of matrix singularity problem, to overcome the instability of the algorithm, at the same time reduced the amount of calculation. And through software simulation and experiment verify the effectiveness of the algorithm[8-10].

For three axial magnetic heading sensor, and its inherent error is mainly characterized by zero error, error sensitivity, orthogonal error, etc. Assume that the actual output of the sensor is $h_{s}$. No error exists for the ideal output is $h_{t}$. $h_{s} \neq h_{t}$, and its mathematical model is expressed as available as
$h_{s}=K_{d} K_{p} h_{t}+B_{e}=K_{e} h_{t}+B_{e}$

Error matrix $K_{d}$ is a third order diagonal matrix, which stands for the sensitivity of various shaft sensor. $K_{p}$ stands for non orthogonality between the axis of sensors and soft magnetic material part. Then a sensor proper reference coordinate system can be established. $K_{p}$ can be presented by third order diagonal matrix. $B_{e}$ stands for sensor's zero error and hard magnetic materials. Error compensation of sensors equal to determine the error coefficient matrix $K_{e}$ and $B_{e}$. By the known actual output $h_{s}$, To solve the ideal output $h_{t}$.
$h_{t}=K_{c}\left(h_{s}+B_{c}\right)$

In Eq.(2), $K_{c}=K_{e}^{-1}, \quad B_{c}=-B_{e}$.
The vector of $h_{t}$ is in the form of:
$\left[\begin{array}{l}h_{x_{t}} \\ h_{y_{t}} \\ h_{z_{t}}\end{array}\right]=\left[\begin{array}{ccc}k_{11} & 0 & 0 \\ k_{21} & k_{22} & 0 \\ k_{31} & k_{32} & k_{33}\end{array}\right]\left(\left[\begin{array}{l}h_{x_{s}} \\ h_{y_{s}} \\ h_{z_{s}}\end{array}\right]+\left[\begin{array}{l}b_{1} \\ b_{2} \\ b_{3}\end{array}\right]\right)$
At a certain moment for a fixed position, and think that the magnetic field strength and the direction is constant.
Rotation of the sensor in three-dimensional space, the ideal output data within the space of trajectory is spherical,

$$
\begin{equation*}
\left\|h_{t}\right\|^{2}=H^{2} \tag{4}
\end{equation*}
$$

$H$ means the location of the magnetic field intensity. Combining Eq. (2) with Eq. (4), we can get:
$h_{s}^{T} A h_{s}-2 b^{T} A h_{s}+b^{T} A b=H^{2}$
$A=K_{c}^{T} K_{c} \quad b=-B_{c}$. Based on the assumption of the ellipsoid compensation approach considers the measurements of the actual output trajectory to ellipsoid, namely Eq. (5) said ellipsoid equation of vector. So, the problem of error compensation of sensors into ellipsoid fitting problem.

Changing Eq. (5) into the general equation of quadric surface, then we can get:

$$
\begin{align*}
F(\alpha, X)= & a_{1} x^{2}+a_{2} x y+a_{3} y^{2}+a_{4} x z+a_{5} y z+ \\
& a_{6} z^{2}+a_{7} x+a_{8} y+a_{9} z+a_{10} \\
= & \alpha^{T} X=0 \tag{6}
\end{align*}
$$

$X=\left[\begin{array}{llllllll}x^{2} & x y & y^{2} & x z & y z & z^{2} & x & y \\ z & z\end{array}\right]^{T} \quad \alpha=\left[\begin{array}{lllll}a_{1} & a_{2} & a_{3} & \cdots & a_{10}\end{array}\right]^{T}$,
The measurement data of ellipsoid fitting is to solve the coefficient of ellipsoid. It is to meet all the sum of the $\arg \min (E)$
squares of the algebraic distance measurement data to the ellipsoid minimum[9], as
$E=\sum_{i=1}^{N} F\left(\alpha, X_{i}\right)^{2}=\|D \alpha\|^{2}$
$D=\left[\begin{array}{llll}X_{1} & X_{2} & X_{3} & \cdots\end{array} X_{N}\right]^{T}$, which is a $N \times 6$ matrix.
In order to guarantee the quadric surface to ellipsoid, to satisfy the following constraints [10],
$\operatorname{det}(W)>0 \Leftrightarrow 4 a_{1} a_{3}-a_{2}^{2}>0$
$\left(a_{1}+a_{3}\right) \operatorname{det}(A)>0$
$W=\left[\begin{array}{cc}a_{1} & a_{2} / 2 \\ a_{2} / 2 & a_{3}\end{array}\right], \quad A=\left[\begin{array}{ccc}a_{1} & a_{2} / 2 & a_{4} / 2 \\ a_{2} / 2 & a_{3} & a_{5} / 2 \\ a_{4} / 2 & a_{5} / 2 & a_{6}\end{array}\right]$
, As the free parameters, $\alpha$ can be chosen suitable magnification, making Eq. (8)satisfy $4 a_{1} a_{3}-a_{2}^{2}=1$.
$\alpha^{T} C \alpha=1$
Solution satisfy the constraint conditions (9-10) of the matrix equation (7), using Lagrange multiplier method available:
$\left\{\begin{array}{l}D^{T} D \alpha=\lambda C \alpha \\ \alpha^{T} C \alpha=1 \\ \left(a_{1}+a_{3}\right) \operatorname{det}(A)>0\end{array}\right.$
Solving the equation (11), coefficient $\alpha_{\text {of ellipsoid for the least positive characteristics of the corresponding }}$ eigenvectors.

## 2. Experiments

According to the special structure of the matrix, through the matrix decomposition, can overcome the defects of constraint matrix is singular, and simplify the feature vector to solve.

Firstly, $D=\left[D_{1} D_{2}\right]$, and

$$
D_{1}=\left[\begin{array}{ccc}
x_{1}^{2} & x_{1} y_{1} & y_{1}^{2} \\
\vdots & \vdots & \vdots \\
x_{i}^{2} & x_{i} y_{i} & y_{i}^{2} \\
\vdots & \vdots & \vdots \\
x_{N}^{2} & x_{N} y_{N} & y_{N}^{2}
\end{array}\right]_{N \times 3} \quad D_{2}=\left[\begin{array}{ccccccc}
x_{1} z_{1} & y_{1} z_{1} & z_{1}^{2} & x_{1} & y_{1} & z_{1} & 1 \\
\vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
x_{i} z_{i} & y_{i} z_{i} & z_{i}^{2} & x_{i} & y_{i} & z_{i} & 1 \\
\vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
x_{N} z_{N} & y_{N} z_{N} & z_{N}^{2} & x_{N} & y_{N} & z_{N} & 1
\end{array}\right]_{N \times 7}
$$

then
$S=D^{T} D=\left[\begin{array}{ll}S_{1} & S_{2} \\ S_{3} & S_{4}\end{array}\right]$, and
$S_{1}=D_{1}^{T} D_{1}, \quad S_{2}=D_{1}^{T} D_{2}, \quad S_{3}=D_{2}^{T} D_{1}=S_{2}^{T}, \quad S_{4}=D_{2}^{T} D_{2}$.
We can get the constrain matrix $C=\left[\begin{array}{ll}C_{1} & C_{2} \\ C_{3} & C_{4}\end{array}\right]$,and $\quad C_{1}=\left[\begin{array}{ccc}0 & 0 & 2 \\ 0 & -1 & 0 \\ 2 & 0 & 0\end{array}\right], \quad C_{2}=[0]_{3 \times 7}, \quad C_{3}=[0]_{7 \times 3}, \quad C_{4}=[0]_{7 \times 7}$.
Making $\alpha=\left[\begin{array}{l}\alpha_{1} \\ \alpha_{2}\end{array}\right]$, and $\alpha_{1}=\left[\begin{array}{lll}a_{1} & a_{2} & a_{3}\end{array}\right]^{T}, \quad \alpha_{2}=\left[\begin{array}{lllll}a_{4} & a_{5} & a_{6} & a_{7} & a_{8}\end{array} a_{9} a_{10}\right]$.
Take the above matrix decomposition into (11), we can get:
$S_{1} \alpha_{1}+S_{2} \alpha_{2}=\lambda C_{1} \alpha_{1}$
$S_{2}^{T} \alpha_{1}+S_{4} \alpha_{2}=0$
When the sampling data is not in the same plane, $S_{4}$ is a singular matrix [12], finishing available:
$C_{1}^{-1}\left(S_{1}-S_{2} S_{4}^{-1} S_{2}^{T}\right) \alpha_{1}=\lambda \alpha_{1}$
$\alpha_{2}=-S_{4}^{-1} S_{2}^{T} \alpha_{1}$

Then Eq.(10) can be changed into
$\alpha_{1}^{T} C_{1} \alpha_{1}=1$

Matrix decomposition above combine Eq, (11) with Eq. (14-16) solution, get the minimum corresponding eigenvectors are characteristic root, and plug in Eq. (9). This formula (11) solving the 10 d feature vector into formula (14) solution of three dimensional feature vector to decrease the amount of calculation for about a third of the original, and at the same time using the improved algorithm on accuracy is consistent with the original algorithm.

According to the Eq.(5-6) matrix $A, ~ b$ can be obtained, and because of the Eq.(10) for amplification coefficient $\alpha$, the matrix is relative. As the absolute value of $A$ magnification by Eq. (5), (6) corresponding relation can be obtained:

$$
\begin{equation*}
k=a_{10} /\left(b^{T} A b-H^{2}\right) \tag{17}
\end{equation*}
$$

Calculated according to the Eq.(17), matrix $A, ~ b$, , and by Eq. (5) to work out the corresponding relationship between error compensation coefficient matrix $K_{c}$ and $B_{c}$, and complete the error compensation[11-12].

In order to validate the above algorithm, simulation software. Assuming that the magnetic sensor location uniform magnetic field, the magnetic field strength of 0.52 Gauss. we divide the ideal output $h_{t}$ spherical area into $N$ regions, each segmented region, random selection of a measuring point data. As shown in figure 1


Figure 1 Plot of recorded data
Set the sensor error coefficient matrix is respectively:

$$
K_{e}=\left[\begin{array}{ccc}
1.1338 & 0 & 0 \\
0.2221 & 1.0537 & 0 \\
0.0392 & -0.3171 & 0.9681
\end{array}\right], \quad B_{e}=\left[\begin{array}{r}
0.0159 \\
-0.0043 \\
0.0016
\end{array}\right] .
$$

Join the variance is 0.0003 gaussian white noise. At each location record ideal vector $h_{t}$ and error of sensor output contains magnetic vector, $h_{s}$ as shown in figure 2.


Figure 2 True magnetic field vector $h_{t}$ and Erroneous measured vector $h_{s}$

Using the above algorithm to ellipsoid, fitting and calculation error compensation coefficient matrix $K_{c}, ~ B_{c}$.
To test algorithm calculation accuracy, with a given magnetic sensor attitude as a benchmark, and the computed error compensation of the magnetic sensor course. Record of location respectively set the pitching Angle and tilt Angle, pitching Angle and tilt Angle, pitching Angle and tilt Angle, pitching Angle and tilt Angle for the round, each group of uniform record 36 points. Calculate the yaw Angle error is shown in figure 3:


Figure 3 Heading error of simulation

## RESULTS AND DISCUSSION

To identify the above method is accurate and reliable, and the error compensation test, magnetic sensor when installation of X and X axis of turntable accurate alignment, Y in the X axis turntable, Y axis in the plane, the turntable from magnetic materials at the same time.

First of all, in accordance with the section method, record the regional sampling point location data. Secondly ellipsoid coefficient is calculated using the fitting method, as shown in table 1, and translated into coefficient matrix and the error compensation $K_{c}, B_{c}$.

Table 1 Parameters of ellipsoid

| $a_{1}$ | $a_{2}$ | $a_{3}$ | $a_{4}$ | $a_{5}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.6060 | -0.2900 | 1.5813 | -0.0171 | 0.0130 |
| $a_{6}$ | $a_{7}$ | $a_{8}$ | $a_{9}$ | $a_{10}$ |
| 1.7931 | 0.0142 | 0.0129 | 0.0191 | -0.2704 |

To test compensation effect, respectively in the pitching Angle $0^{\circ}$ and tilt Angle $0^{\circ}$, pitching Angle $0^{\circ}$ and tilt Angle $30^{\circ}$, pitching Angle $30^{\circ}$ and tilt Angle $0^{\circ}$, pitching Angle $30^{\circ}$ and tilt Angle $30^{\circ}$ for the state, the use of
non-magnetic turntable as a reference benchmark, within the scope of the $0^{\circ}{ }_{-} 360^{\circ}$ of course, interval record $10^{\circ}$ heading sensor output data, the heading error of measuring magnetic sensor. Before and after the compensation yaw Angle error is shown in figure 4. Compensation before you can see, the maximum error of the yaw Angle $5.92^{\circ}$, compensation does not exceed the maximum error of $0.42^{\circ}$.


Figure 4 Errors at different points

## CONCLUSION

Puts forward the improved ellipsoid based on the least square fitting method of magnetic heading sensor error compensation method, through analyzing the singularity of the constraint matrix, to overcome the instability problem of traditional ellipsoid fitting method, and the software simulation and experimental validation. This method can compensate the sensor's zero error, error sensitivity, orthogonal error such as inherent error, without external reference benchmark. On the non-magnetic turntable experiments showed that the maximum error of magnetic heading is not more than $0.42^{\circ}$, feasibility and accuracy of this method is verified by the experiments.

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